Test Report issued under the responsibility of: Shenzhen TCT Testing Technology Co., Ltd.

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0	C)	TEST REPOR IEC 60255-15	₹T 51		(C)
	Measuring	relays and protect	tion equiper	nent –	
Part	151: Functional	requirements for o	ver/under c	urrent protec	tion
Report Number		TCT231016S007			
Date of issue	<u> (</u> <u> (</u>	2023-11-01			
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Applicant's nan	:	Primus Co., Ltd.			
Address		119 Soi Srimuang Ar Bangkkok 10400 TH/	iusorn, Sutthisa AILAND	arnvinijchai Rd.,	Dindaeng,
Test specification	on:				
Standard	:	IEC 60255-151:2009)		
Test procedure	.)	IEC test report			
Non-standard te	est method: :	N/A			
Test Report For	m No:	IEC 60255-151			
Test Report For	m(s) Originator :	тст			
Master TRF		Dated 2023-03-23			
The International comprising all na promote internati fields. To this end Specifications, Te as "IEC Publication interested in the non-governmenta closely with the In determined by ag	Electrotechnical Con tional electrotechnica onal co-operation on and in addition to ot echnical Reports, Put on(s)"). Their prepara subject dealt with may al organizations liaisin thernational Organiza greement between the	nmission (IEC) is a work I committees (IEC Natio all questions concerning her activities, IEC publis blicly Available Specifica- tion is entrusted to tech y participate in this prep ng with the IEC also part tion for Standardization e two organizations.	dwide organiza nal Committee g standardizatio shes Internation ations (PAS) an nical committee aratory work. In ticipate in this p (ISO) in accord	tion for standard s). The object of on in the electrica hal Standards, Te d Guides (herea es; any IEC Nation hternational, gov preparation. IEC dance with condi	lization IEC is to al and electronic echnical fter referred to onal Committee ernmental and collaborates tions
General disclair	ner:			_	
The test results p This report shall i Laboratory. The a	resented in this report not be reproduced, ex authenticity of this Te	rt relate only to the object cept in full, without the st Report and its content	ct tested. written approva its can be verifi	al of the Issuing (ed by contacting	CB Testing the NCB,



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Test item description:	GROUI	ND FAULT PROTE	CTION RELAY	
Trade Mark(s)	PM			
Manufacturer:	Same a	as applicant		
Model/Type reference	VPM-0	8 Series		
Ratings	Power	Supply: 90-250 VA	C/VDC, Max.5A~ CAT II	
Responsible Testing Laboratory (as ap	plicab	le), testing proced	lure and testing location	n(s):
CB Testing Laboratory:)	Shenzhen TCT Te	sting Technology Co., Lto	
Testing location/ address	:	2101 & 2201, Zher Zone, Fuhai Subdi Guangdong, China	nchang Factory, Renshar strict, Bao'an District, She	n Industrial enzhen,
Tested by (name, function, signature).	:	Mick Li	AND TEG	
Approved by (name, function, signatur	e):	Thomas	the	
Testing procedure: CTF Stage 1:				
Testing location/ address	:			
Tested by (name, function, signature).	:			(,0
Approved by (name, function, signatur	e):			
Testing procedure: CTF Stage 2:		G		()
Testing location/ address	:		C	
Tested by (name, function, signature).				
Witnessed by (name, function, signatu	re).:			(Å
Approved by (name, function, signatur	e):		×	C
Testing procedure: CTF Stage 3:				<u></u>
Testing procedure: CTF Stage 4:		K		
Testing location/ address	:			
Tested by (name, function, signature).	:			
Witnessed by (name, function, signatu	re).:		(\mathbf{C})	(C)
Approved by (name, function, signatur	e):			
Supervised by (name, function, signate	ure) :			
			/ ~)



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Copy of marking plate:

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Test item particulars:				
Product group	:	ind product	built-in component	
Classification of use by Mass of equipment (kg)	:) 	 Ordinary person Instructed person Skilled person 0.18 kg 	Children like	ly present
Possible test case verdicts:				
 test case does not apply to test object does meet the r 	o the test object: requirement:	N/A P (Pass)		
 test object does not meet t 	he requirement:	F (Fail)		
Testing: Date of receipt of test item .	<u>)</u>	2023-10-16		
Date (s) of performance of te	ests:	2023-10-16 to 2023-1	1-01	
General remarks:	(¿G`)	(¿G`)	(° O x)	
"(See Enclosure #)" refers to "(See appended table)" refers IEC-60255-151 replaces IEC Throughout this report a The related applicable CTL de	additional informatic to a table appended -60255-4(expired). comma / poin ecisions have been c	on appended to the report to the report. In tis used as the decir onsidered and the requi	ort. mal separator. irements found fulfilled.	Ś
Manufacturer's Declaration	per sub-clause 4.2.	5 of IECEE 02:		
The application for obtaining a includes more than one factor declaration from the Manufact sample(s) submitted for evaluative of the products has been provided	a CB Test Certificate y location and a urer stating that the ation is (are) from each factory	☐ Yes☑ Not applicable		
When differences exist; the	y shall be identified	in the General produc	ct information section.	
Name and address of factor	ry (ies) :	Same as manufacture	er.	
General product informatio 1. All the models are identica	n and other remark I to testing model ex	(s: cept for model name.		Ś

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Clause	Requirement + rest		Veruici
4	Specification of the function		Р
4.1	General		Р
	The protection function with its inputs, outputs, measuring element, time delay characteristics and functional logic is shown in Figure 1. The manufacturer shall provide the functional block diagram of the specific implementation		Ρ
	Functional logic Threshold(s)	1	Ρ
4.2	Input Energizing quantities / energizing quantities		Ρ
	The input energizing quantities are the measuring signals, e.g. currents and voltages (if required). Their ratings and relevant standards are specified in IEC 60255-1. Input energizing quantities can come with wires from current and voltage transformers or as a data packet over a communication port using an appropriate communication protocol (such as IEC 61850-9-2)		Ρ
	The energizing quantities used by the protection function need not be directly the current at the secondary side of the current transformers. Therefore, the measuring relay documentation shall state the type of energizing quantities used by the protection function. Examples are:		Ρ
	single phase current measurement;		Р
	three phase current measurement;		N/A
	• neutral current or residual current measurement;		N/A
	positive, negative or zero sequence current measurement.		N/A
	The type of measurement of the energizing quantity shall be stated. Examples are:		Ρ
	• RMS value of the signal;		Р
	RMS value of the fundamental component of the signal;		N/A
	• RMS value of a specific harmonic component of the signal;		N/A
	• peak values of the signal;		N/A

Page 7 of 30 Report No.:TCT231016S007 IEC 60255-151 Requirement + Test Result - Remark Verdict Clause · instantaneous value of the signal. N/A 4.3 **Binary input signals** Ρ If any binary input signals (externally or internally Ρ driven) are used, their influence on the protection function shall be clearly described on the functional logic diagram. Additional textual description may also be provided if this can further clarify the functionality of the input signals and their intended usage. **Functional logic** Ρ 4.4 4.4.1 **Operating characteristics** Ρ 4.4.1.1 Ρ General The relationship between operate time and Ρ characteristic quantity can be expressed by means of a characteristic curve. The shape of this curve shall be declared by the manufacturer by an equation (preferred) or by graphical means This standard specifies two types of characteristics: Ρ Р · independent time characteristic (i.e. definite time delay); · dependent time characteristic (i.e. inverse time N/A delay). The time characteristic defines the operate time Ρ which is the duration between the instant when the input energizing quantity crosses the setting value (G_s) and the instant when the relay operates. 4.4.1.2 Ρ Independent time characteristic Independent time characteristic is defined in terms Ρ of the setting value of the characteristic quantity G_s and the operate time top. When no intentional time delay is used, then the independent time relay is denoted as an instantaneous relay. For overcurrent relays, $t(G) = t_{op}$ when $G > G_S$. The Ρ independent time characteristic is presented in Figure 2. Ρ *t*(G) IEC 1706/09 Figure 2 - Overcurrent independent time characteristic



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	For undergurrent relays $t(C) = t$, when $C < C$		
	The independent time characteristic is presented in Figure 3.		
	((G) t _{op} G ₈ G ₈ G ₈ (C) IEC 1707/09		Ρ
	Figure 3 – Undercurrent independent time characteristic		
4.4.1.3	Dependent time characteristics		N/A
	Dependent time characteristics are only defined for overcurrent relays.		N/A
	For dependent time relays the characteristic curves shall follow a law of the form:		N/A
	$t(G) = TMS\left[\frac{k}{\left(\frac{G}{G_{S}}\right)^{\alpha} - 1} + c\right]$		N/A
	where t(G) is the theoretical operate time with constant value of G in seconds; k, c, α are the constants characterizing the selected curve; G is the measured value of the characteristic quantity; G _S is the setting value (see 3.3); TMS is the time multiplier setting (see 3.1 0). The constants, k and c, have a unit of seconds, α has no dimension.		
	The dependent time characteristic is shown in Figure 4.		N/A
		\sim	

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	r(G) (G) (G) (G) (G) (G) (G) (G)		N/A
	Figure 4 – Dependent time characteristic		
	The effective range of the characteristic quantity for the dependent time portion of the curve shall lie between $2 \times G_S$ and G_D . The minimum value of G_D is equal to 20 times the setting value G_S . The manufacturer shall declare the setting value range for which this is applicable. For setting values higher than this range, the manufacturer shall declare the value of G_D .	r	N/A
	The threshold value G_T is the lowest value of the input energizing quantity for which the relay is guaranteed to operate. G_T lies between G_S and		N/A
	$1,3 \times G_S$. Its value shall be defined by the manufacturer.		
	Dependent time relays shall have a definite minimum operate time. This requirement may be defined by assigning a definite time delay for currents above a given energizing quantity level. Alternatively, the manufacturer can make the dependent time relay behaviour to cease for levels of energizing quantity in excess of a specified value (G_D/G_S), as described by the following equation:	9	N/A
	For $G > G_D$ $t(G) = TMS \cdot \left(\frac{k}{\left(\frac{G_D}{G_S}\right)^{\alpha} - 1} + c\right)$		N/A
	where		

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	G _D is the level of the characteristic quantity at which dependent time operation ceases and independent time operation commences (see		
	t(G) is the theoretical operate time with constant value of G in seconds;		
	k, c, α are constants characterizing the selected curve;		
	G is the measured value of the characteristic quantity;		
	G sis the setting value (see 3.3);TMSis the time multiplier setting (see 3.1 0).		
	There are six curves denoted as A, B, C, D, E and F whose coefficients for Equations (1) and (2) shall be from Annex A. The manufacturer shall declare which of these curves are implemented and state the values of G_D and G_T		N/A
	Power system fault conditions can produce time varying currents. To ensure proper coordination between dependent time relays under such conditions, relay behaviour shall be of the form described by the integration given by Equation 3.		N/A
	For G > Gs		N/A
	$\int_{0}^{T_0} \frac{1}{t(G)} dt = 1$		
	where T_0 is the operate time where G varies with		
	time; t(G) is the theoretical operate time with constant value of G in seconds:		
	G is the measured value of the characteristic quantity.		
	Operate time is defined as the time instant when the integral in Equation (3) becomes equal to		N/A
442	Reset characteristics		P
4421	General		, P
→... . I	To allow users to determine the behaviour of the relay in the event of repetitive intermittent faults or for faults which may occur in rapid succession, relay reset characteristics shall be defined by the manufacturer. Different reset characteristics may be used depending upon the settings on the relay and whether the element has completed operation or not. The recommended reset characteristics are defined below		P

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	The manufacturer shall declare if compensation of the internal measurement time (disengaging time) is included in the reset time.		P	
4.4.2.2	No intentional delay on reset		N/A	
	For G < (reset ratio) x Gs. the relay shall return to its reset state with no intentional delay as declared by the manufacturer. This reset option can apply to both dependent and independent time relays		N/A	
4.4.2.3	Definite time resetting		N/A	
	Generally, this reset characteristic is applicable to overcurrent protection.		N/A	
	For G < (reset ratio) x Gs, the relay shall return to its reset state after a user-defined reset time delay, t_r . During the reset time, the element shall retain its state value as defined by $\int_{0}^{t_p} \frac{1}{t(G)} dt$ with t_p being the transient period during which G > G _S . If during the reset time period, the characteristic quantity exceeds G _S , the reset timer t_r . is immediately reset to zero and the element continues normal operation starting from the retained value	n	N/A	
	Following G > G_S for a cumulative period causing relay operation, the relay shall maintain its operated state for the reset time period after the operating quantity falls below Gs as shown in Figure 5. Alternatively, the relay may return to its reset state with no intentional delay as soon as the operating quantity falls below Gs after tripping as shown in Figure 6.	b	N/A	
	This reset option can apply to both dependent and independent time elements. A graphical representation or this reset characteristic is shown in Figures 5 and 6 for partial and complete operation of the element.		N/A	
	Energising Quantity > Ge Start (pick-up) Signal Value of internal time delay setting value of value of	-	N/A	
<u></u>				



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		1	1
	curve; G is the measured value of the characteristic quantity; Gs is the setting value (see 3.3); TMS is the time multiplier setting (see 3.10).		
	For the curves A, B, C, D, E, F previously defined, the value of t _r , shall be in accordance with Annex A.		N/A
	Figure 7 illustrates the effect of the dependent time reset on the internal time delay counter Following $G > G_S$ for a cumulative period causing relay operation, when the operating quantity falls below G_S , the relay shall return to its reset state after the time t _R (G). Alternatively, the relay may return to its reset state with no intentional delay as shown in Figure 8. The behaviour of reset time after relay operation shall be described		N/A
	Energising quantity > G Start (pick-up) signal Operate signal Operate signal Operate level_b of the nitegrator Value of integrator) Value of integrator Preset time Charter to be setting (with G = 0. TMS = 1) Reset time Figure 7 – Dependent time reset characteristic		N/A
	Figure 8- Dependent time reset characteristic (alternative solution with instantaneous reset after relay operation)		P
4.5	Binary output signals		Р
4.5.1	Start (pick-up) signal		Р
	The start signal is the output of measuring and threshold elements, without any intentional time delay. If a start signal is not provided the manufacturer shall give information on how to conduct testing related to start signal as defined in Clause 6		P

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4.5.2	Operate (trip) signal		Р
	The operate signal is the output of measuring and threshold elements, after completion of any intentional operating time delay. In the case of instantaneous elements, this signal may occur at the same time as the start signal (if provided).		P
4.5.3	Other binary output signals		Р
	If any binary output signals are available for use, their method of operation shall be clearly shown on the functional logic diagram. Additional textual description may also be provided if this can further clarify the functionality of the output signal and its intended usage		P
4.6	Additional influencing functions/conditions		N/A
	The manufacturer shall declare if any specific algorithms are implemented in the relay, for example:		N/A
	insensitive to inrush current;		N/A
	• cold load pickup;		N/A
	• insensitive to false residual current due to phase current transformer saturation (when the residual current is measured with 3 phase current transformers);		N/A
	second harmonic blocking/restrain feature		N/A
	The performances of these specific characteristics shall be described		N/A
4.7	Specific characteristics		N/A
	The setting value (pick-up) of voltage-dependent overcurrent protection is adjusted according to the voltage measured (phase-to-phase voltage or phase-to-neutral voltage). The adjusted setting is equal to the original setting, G_s , multiplied by a coefficient β , defined by the following two characteristics, as shown in Figures 9 and 1 0. U is the voltage applied to relay in volts and U_n is the rated voltage in volts. The manufacturer shall declare the available values for k1 k2 k3 k4		N/A
KU)		Ko)	- Ko

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	For both dependent and inc the manufacturer shall decl to the characteristic quantit value range over which it is the manufacturer shall also performance of the elemen conditions (at thermal short such as current = 100 × rat	dependent time relays, are the accuracy related y along with a setting applicable. In addition, declare the t under high fault current t-time withstand limit ed current).		P
	For functions with a voltage manufacturer shall declare accuracy related to the volt the combination of a varyin and a varying voltage, it is accuracy of the voltage dep voltage range for one given	e dependent element, the additionally the age. In order to avoid g characteristic quantity sufficient to specify the pendency in the specified y value of G ₂ at nominal		N/A

	accuracy of the voltage dependency in the specified voltage range for one given value of $G_{\rm s}$ at nominal current ($I_{\rm N}$).	
5.2	Accuracy related to the operate time	Р
	For independent time relays, the maximum permissible error of the specified operate time shall be expressed as either:	Р
	 a percentage of the time setting value, or; 	Р
	• a percentage of the time setting value, together with a fixed maximum time error (where this may exceed the percentage value), whichever is greater. For example, \pm 5% or \pm 20 ms whichever is greater, or;	Ρ
	• a fixed maximum time error.	N/A
	For dependent time relays, the reference limiting error is identified by an assigned error declared by the manufacturer, which may be multiplied by factors corresponding to different values of the characteristic quantity. For relays with a decreasing time function, the value of the assigned error shall be declared at the maximum limit of the effective range of the dependent time portion of the characteristic (G_D) as a percentage of the theoretical time. The reference limiting error shall be declared either as:	N/A
	• a theoretical curve of time plotted against multiples of the setting value of the characteristic quantity bounded by two curves representing the maximum and minimum limits of the limiting error over the effective range of the dependent time portion of the characteristic, or;	N/A
	• an assigned error claimed at the maximum limit of the effective range of the dependent time portion of the characteristic multiplied by stated factors corresponding to different values of the characteristic quantity within its effective range of the dependent time portion of the characteristic, as specified in Table 1.	N/A

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	Table 1 – Multiplier factor on operated time assigned error Value of characteristic quantity as multiple of setting value (G_s) 2 – 5 5 – 10 10 – G_0 Limiting error as multiple of an assigned error 2.5 1.5 1	N/A
	For both dependent and independent time relays, the manufacturer shall declare the maximum limiting error related to the operate time along with a setting range of time delay over which it is applicable.	N/A
	The manufacturer shall declare if the internal measurement time of the characteristic quantity and the output contact operation time is included in the time delay setting or if it is in addition to the time delay setting.	N/A
5.3	Accuracy related to the reset time	Р
	For relays with no intentional reset delay, the manufacturer shall declare the reset time of the element.	N/A
	For relays with a definite time delay on reset, the maximum permissible error of the specified reset time shall be expressed as either	N/A
	• a percentage of the reset time setting value, or;	N/A
	• a percentage of the reset time setting value, together with a fixed maximum time error (where this may exceed the percentage value), whichever is greater. For example, \pm 5% or \pm 20 ms whichever is greater, or;	N/A
	• a fixed maximum time error.	N/A
	For relays with a dependent time delay on reset, the maximum permissible error is identified by an assigned error declared by the manufacturer, which may be multiplied by factors corresponding to different values of the characteristic quantity. For relays with a decreasing time function, the value of the assigned error shall be declared at the reference condition as a percentage of the theoretical time. The maximum permissible error shall be declared either as:	Ρ
	• a theoretical curve of time plotted against multiples of the setting value of the characteristic quantity bounded by two curves representing the maximum and minimum limits of the permissible error, or;	Ρ
	• an assigned error claimed at the reference condition, multiplied by stated factors corresponding to different values of the characteristic quantity, as specified in Table 2	Р
	Table 2 – Multiplier factor on reset time assigned error Value of characteristic quantity as multiple of setting value (G_8) $0.8 - 0.4$ $0.4 - 0.2$ $0.2 - 0.1$ Limiting error as multiple of an assigned error 2.5 1.5 1	P
	For both dependent and independent time relays, the manufacturer shall declare the maximum limiting	Р

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L			
	error related to the reset time along with a setting range of time delay over which it is applicable		
	The manufacturer shall declare if the internal measurement time (disengaging time) is included in the reset time setting or if it is in addition to the reset time setting.		P
5.4	Transient performance		N/A
5.4.1	Transient overreach		N/A
	For independent time overcurrent protection, the manufacturer shall declare as a percentage error of start value (G_S) the effect of applying waveforms with maximum d.c. offset associated with systems having an X/R ratio up to 120 (primary time constant of 380 ms at 50 Hz or 320 ms at 60 Hz).		N/A
5.4.2	Overshoot time		N/A
	The manufacturer shall declare the overshoot time.		Р
5.4.3	Response to time varying value of the characteristic quantity		Р
	To ensure proper coordination with dependent lime relays, the relay performance under time varying fault current conditions (characteristic quantity varies with time) shall be tested. The manufacturer shall declare any additional errors, but in all cases, the additional error shall be less than 15 %		P
5.5	Current transformer requirements		Р
	The manufacturer shall provide guidance on the class and sizing of the current transformers (refer to IEC 60044 series of standards).		Р
6	Functional test methodology		Р
6.1	General		Р
	Tests described in this clause are for type tests. These tests shall be designed in such a way as to exercise all aspects of hardware and firmware (if applicable) of the over/under current protection relay. This means that injection of current shall be at the interface to the relay, either directly into the conventional current transformer input terminals, or an equivalent signal at the appropriate interface. Similarly, operation shall be taken from output contacts wherever possible or equivalent signals at an appropriate interface.		P
	If for any reason it is not possible to measure the results from signal input to output, the point of application of the characteristic quantity and the signal interface used for measurement shall be declared by the manufacturer. For relays where the settings are in primary values one current transformer ratio can be selected for performing the		P

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	tests	
	In order to determine the accuracy of the relay in steady state conditions, the injected characteristic quantity shall be a sinusoid of rated frequency and its magnitude should be varied according to the test requirements.	Р
	Some of the tests described in the following subclauses can be merged to optimize the test process. Depending upon the technology of the relay being tested, it may be possible to reduce the number of test points in line with the limited range and step-size of available settings. However, the test points listed should be used or the nearest available setting if the exact value can not be achieved.	Р
	In the following subclauses, the test settings to be used are expressed in a percentage of the available range with 0 % representing the minimum available setting and 100 % representing the maximum available setting. Similarly 50 % would represent the mid-point of the available setting range. The actual setting to be used can be calculated using the following formula:	Ρ
	$S_{AV} = (S_{MAX} - S_{MIN})X + S_{MIN}$ where S_{AV} is the actual setting value to be used in the test; S_{MAX} is the maximum available setting value; S_{MIN} is the minimum available setting value; X is the test point percentage value expressed in the test methodology (see Tables 3, 4, 5 and 6).	Ρ
	For example, for the operating current setting in Table 5, assuming the available setting range is 0,1 A to 4,0 A, the actual operating current settings to be used would be: 0,10 A; 2,05 A; 4,00 A.	N/A
	The following subclauses refer to a rated current of the relay and it is denoted as I_n .	N/A
6.2	Determination of steady state errors related to the characteristic quantity	Р
6.2.1	Accuracy of setting (start) value	Р
	In order to determine the accuracy of the setting value (G $_{\rm S}$) the characteristic quantity (magnitude) should be varied slowly and the start output of the element monitored for operation. For overcurrent protection, the characteristic quantity shall be increased according to the criteria below:	Ρ
	• The initial value of the characteristic quantity shall be below the setting value by at least 2 times the specified accuracy of the element.	Р

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	• The ramping steps shall be at least 10 times smaller than the accuracy specified for the element		Р
	• The step time shall be at least twice the specified start time value and not more than 5 times the specified start time value.		Р
	EXAMPLE		N/A
	If the setting value is 1 A, accuracy \pm 10% and start time 20 ms, the initial ramp start value is 0,8 A, ramp step size of 0,01 A, with a step time of 40 ms to 100 ms.		N/A
	For undercurrent protection, the characteristic quantity shall be decreased from an initial value which is above the start value by at least twice the specified accuracy of the element. The ramping process is similar to the overcurrent protection.		N/A
	 Sufficient test points should be used to assess the performance over the entire setting range of the element but as a minimum 1 0 settings shall be used with a concentration towards lower start settings where errors are relatively more significant. Preferred values are: minimum setting (or 0 % of the range); 0,5 %; 1 %; 2 %; 3 %; 5 %; 10 %; 30 %; 60 %; maximum setting (or 100 % of the range). 		N/A
	For an overcurrent relay, each test point shall be repeated at least 5 times to ensure repeatability of results, with the maximum and average error values of all the tests being used for the accuracy claim. Additional checks shall be performed at maximum setting value selected to ensure operation occurs for a current value near the short-time thermal withstand limit (such as 100 × rated current) applied to the relay.		N/A
	For an undercurrent relay, each test point shall be repeated at least 5 times to ensure repeatability of results, with the maximum and average error values of all the tests being used for the accuracy claim.		N/A
	The accuracy of the voltage dependent element is tested for a given setting of Gs for a definite time characteristic. The manufacturer has to specify the chosen value of Gs. The values for the factors k1, k2, k3, k4 shall be specified.		N/A
	Example values:		N/A
	• characteristic as in Figure 9: k1 =0,25; k2=0,25; k3=1,0.		N/A
	• characteristic as in Figure 10: k1 = 1 ; k2=0,8; k3=0,8; k4 = infinity (function disabled) or highest possible setting.		N/A
	The accuracy of the voltage dependent element is tested for the following points:		N/A

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Clause	Requirement + Test	Result - Remark	Verdict
	• characteristic as in Figure 9: U/U N =0,8×k2; k2; 0,5×(k2+k3); k3; 1,1×k3		N/A
	• characteristic as in Figure 1 0: U/U N =0,8×k2; 1,1 ×k2		N/A
	In order to determine the accuracy of the voltage dependent element, the characteristic quantity G $_{\rm s}$ is varied slowly with a fixed voltage according to the tested point in the voltage characteristic. The start output of the element monitored for operation. The characteristic quantity is increased according to the criteria below:		N/A
	• The initial value of the characteristic quantity shall be below the setting value by at least 2 times the specified accuracy of the element.		N/A
	• The ramping steps shall be at least 10 times smaller than the accuracy specified for the element.		N/A
	• The step time shall be at least 2 times the specified value and not more than five times the specified value.		N/A
	The error of the voltage dependent element is then calculated as:		N/A
	$G - \beta \times G_s$ where G is the value of the characteristic quantity where the start output is activated; β is taken from Figures 9 or 1 0 according to the applied voltage U/U N		N/A
	For the calculation of relative errors, G s is used as a reference instead of $\beta \times G$ s in order to avoid increasing values resulting from low values for β		N/A
	Each test point shall be repeated at least 5 times to ensure repeatability of results, with the maximum and average error values of all the tests being used		N/A

	ensure repeatability of results, with the maximum and average error values of all the tests being used for the accuracy claim.	
6.2.2	Reset ratio determination	Ρ
	In order to determine the reset ratio, the element shall be forced to operate, and then the characteristic quantity should be varied slowly while monitoring the output of the element with no intentional delay on reset. For overcurrent protection, the characteristic quantity shall be decreased according to the criteria below:	Ρ
	• The initial value of the characteristic quantity shall be above the start value by at least 2 times the specified accuracy of the element.	Ρ

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	• The ramping steps shall be at least 10 times smaller than the accuracy specified for the element.		P
	• The step time shall be at least 2 times the specified disengaging time value and not more than 5 times the specified disengaging time value		Р
	If reset doesn't occur within the time interval, the element is considered to have not reset and, the next lower value of current shall be used.		Р
	EXAMPLE		N/A
	If the setting value is 1 A, accuracy \pm 10 % and disengaging time 20 ms the initial ramp startvalue is 1,2 A, ramp step size of 0,01 A with a step time of 40 ms to 100ms.		N/A
	For undercurrent protection, the characteristic quantity shall be increased from an initial value which is below the start value by at least 2 times the specified accuracy of the element. The ramping process is similar to the overcurrent protection.		N/A
	The rest ratio shall be calculated as follows:		N/A
	Reset ratio (%) = $(I_{reset}/I_{start}) \times 100$		
	where I $_{\text{start}}$ is the start value of the current and I reset is the reset value of the current.		
	Sufficient test points should be used to assess the performance over the entire setting range of the element, but as a minimum ten settings shall be used, with a concentration towards lower start settings where errors are relatively more significant. Preferred values are: minimum setting (or 0 % of the range); 0,5 %; 1 %; 2 %; 3 %; 5 %; 10 %; 30 %; 60 %;maximum setting (or 100 % of the range).		P
	For overcurrent relay, each test point shall be repeated at least 5 times to ensure repeatability of results, with the minimum and average values of all the tests being used for the accuracy claim.		P
	For undercurrent relay, each test point shall be repeated at least 5 times to ensure repeatability of results, with the maximum and average values of all the tests being used for the accuracy claim.		P
6.3	Determination of steady state errors related to the start and operate time		Р

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	In order to determine the steady state errors of the operate time, current shall be applied to the relay with no intentional delay and no d.c. component, and the start and operate output contacts of the element monitored. The switching point of the current from initial test value to end test value shall be at the zero crossing of the waveform. Tests shal be conducted on an individual phase basis. Sufficient test points should be used to assess the performance over the entire time delay or time multiplier setting range, at various operating current values and throughout the effective range of the dependent time portion of the characteristic. Each test point shall be repeated at least 5 times to ensure the repeatability of results, with the maximum and average value of the five attempts being used for the analysis. The times recorded for the operating time accuracy, whilst the times recorded for the start output contact provides a measure of the operating time accuracy. The times recorded for the start time. The following test points, Table 3 for overcurrent elements and Table	l l	P

	4 for undercu	ırrent elemen	I.		
	Та	Table 3 – Test points for overcurrent elements			F
	Operate time or TMS setting	Operating current setting	Initial test current value	End test current value	•
	Minimum (0 %)	Minimum (0 %)	0	1,2 × G _Y	1
	50 %	50 %	0	2 × G _s	i i
	Maximum (100 %)	Maximum (100 %)	0	5 × G _s	i i
	-		0	10 × G _S	I.
	-	-	0	20 × G _s	I.
	Operating time or TM	able 4 – Test points fo	r undercurrent eleme	End test current value	F
	setting	setting	value		I.
	Minimum (0 %)	Minimum (0 %)	2 × G _S	0,8 × G _S	I.
	50 %	50 %	2 × G _S	0,4 × G _S	I.
	Maximum (100 %)	Maximum (100 %)	2 × G _S	0,2 × G _S	I.
		-	2 × 05	0,1 × 05	I.
	NOTE Some relays m to zero, or below a set be reduced to ensure th	ay block operation of the un threshold. In this case, the in the tests are only perform	dercurrent element when the number of test cases that a ned when the undercurrent	he injected current is equal are used from this table will element remains enabled.	
6.4	Determination the reset times times the reset	on of steady ne	state errors	s related to	F
	In order to determine the steady state errors of the reset time, current shall be applied to the relay to cause element operation. With operation complete, the current applied to the relay shall be stepped to the initial test current value for one second, and			P	

then stepped to the end test current value with no intentional delay and a suitable output contact of the element monitored. If an output contact is not available, then the procedure described in Annex B can be applied to determine the reset time of the

relay.

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Clause	Requirement	+ Test			Result - Remark	Verdict
Sufficient test points should performance over the entire reset time multiplier setting r operating current values and effective range of the depen- characteristic. Each test poir least 5 times to ensure the re with the maximum and avera attempts being used for the recorded by monitoring the s measure of the disengaging whilst other suitable signals measure of the reset time ac test points, Table 5 for overce			Id be used to re reset time g range, at v and througho endent time oint shall be repeatabilit erage value the analysis. The start contain ng time of the ls shall be us accuracy. The ercurrent ele elements, are	assess the delay or arious ut the portion of the repeated at y of results, of the five The time ct provides a e element, sed to give a he following ments and e suggested.		P
	Ta Reset time or reset TMS setting Minimum (0 %) 50 % Maximum (100 %) - - NOTE The first column of	ble 5 – Test points fo Operating current setting Minimum (0 %) 50 % Maximum (100 %) - - of this table is not applicable	Initial test current value $2 \times G_{s}$ $2 \times G_{s}$		P	
	Tab Reset time or reset TMS setting Minimum (0 %) 50 % Maximum (100 %) - - NOTE 1 The first column NOTE 2 Some relays m equal to zero, or below a will be increased to ensu- enabled.	ble 6 - Test points for Operating current setting Minimum (0 %) 50 % Maximum (100 %) - - n of this table is not applica hay block operation of the set threshold. In this case ure that the tests are only	r undercurrent eleme Initial test current value 0 0 0 0 ble to relays with no intent undercurrent element with the initial test current use performed when the und	End test current value $1.2 \times G_{T}$ $2 \times G_{S}$ $5 \times G_{S}$ $10 \times G_{S}$ $20 \times G_{S}$ ional delay on reset. nen the injected current is ed in column 3 of this table ercurrent element remains		P
6.5	Determinatio	on of transie	nt performa	ince		N/A
6.5.1	General					N/A
	The transient performance tests are performed at reference conditions where the setting value is $G_s = 1 \times I_n$.				N/A	
6.5.2	Transient ov	erreach				N/A
	This test is designed to view the effect of an offset waveform on the start value accuracy of the element. With the relay setting G_S set to reference conditions, current shall be applied (with no offset) starting at $0.9 \times G_S$ and then increasing until starting just occurs. The current magnitude shall then be reduced by 2 % and then re-applied to the relay to ensure that relay starting does not occur when the current is stepped from 0 A to the test magnitude (starting current minus 2 %). A similar test may also be performed such that a step from 0 A to the test current plus 2 % causes operation.				N/A	

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	With the test current magnitude established, tests shall be performed with the maximum d.c. offset present and with a constant X/R ratio up to 120 (preferred test points are for X/R ratios of 10, 40 and 120). Typical test waveform is shown in Figure 11 for a 50 Hz nominal frequency. During the tests, current shall be stepped from 0 A to the test current magnitude with no intentional delay, and relay operation shall be monitored for at least the duration of the time constant of the current waveform. If the element starts to operate, the test shall be re-performed with a higher setting for G s until application of the offset waveform does not cause relay starting. Five successive non-operations for a given setting value indicate that the transient overreach stability point has been reached.		N/A
	The transient overreach at each X/R value is given by:		N/A
	Transient overreach (in %) = $\left(\frac{\text{Setting at which no operation occurs for offset waveform}}{\text{Setting at which no operation occurs for waveform without offset}} -1\right) \times 100$		N/A
	Image: constraint of the second se		N/A
6.5.3	Overshoot time		N/A
	Overshoot time is relevant for overcurrent relay and it is not applicable for undercurrent relay.		N/A
	With the relay setting at reference conditions (setting value of I n), current shall be switched from an initial value of zero to $5 \times G_S$ and the relay operate time shall be measured as a maximum value out of five attempts. With this known operating time, the same current of $5 \times G_S$ shall be applied for a period of time 5 ms less than the maximum operate time and then reduced to zero with no intentional delay. If relay operation occurs, the period of time for which the current is injected shall be reduced by a further 5 ms, and the test shall be performed again. The injection time shall be decreased further until five successive injections of current do not cause the relay to operate.		N/A

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	The difference in time between the current injection period and the measured relay operate time is the relay overshoot time.		N/A
	For an independent time overcurrent relay, a current of $2 \times G_S$ shall be used instead of $5 \times G_S$ and a time delay of 200 ms shall be used for this test. Overshoot time test is not required for an instantaneous overcurrent function.		N/A
6.5.4	Response to time varying value of the characteristic quantity for dependent time relays		N/A
	The test waveform or the characteristic quantity is shown in Figure 12, which represents a 50 Hz or 60 Hz waveform modulated by a square wave so that the changes in magnitude or the sine-wave occur at zero crossings.		N/A
	$\int_{IEC} \frac{3_2\sqrt{2}}{1716/09}$ Figure 12 – Test waveform		N/A
	The frequency of the modulating square-wave shall not be higher than 1/10 of the main frequency, so that the transient behaviour of the relay does not affect the operate time.		N/A
	The magnitudes G $_1$ and G $_2$ of the characteristic quantity are both above G $_s$, the setting value of the characteristic quantity. The magnitudes are selected so that the operate time of the relay is much greater than the period of the modulating square wave.		N/A
	With the above conditions, the theoretical operate time T_0 is: $T_0 = \frac{2 \times T_1 \times T_2}{T_1 + T_2}$		N/A
	where T_1 is the operate time for characteristic quantity equal to G_1 ; T_2 is the operate time for characteristic quantity equal to G_2		
	Recommended values for the time varying characteristic quantity are given in Table 7 where the frequency of the modulating square-wave is 1 /1 0 of the main frequency. With values of Table 7, the measured operate time shall not differ from T_0 by more than 15 %.		N/A

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[Та	ible 7 – Recorr	mended value	as for the tes	t			NI/A
	Curve	TMS	G1	G2	τ ₁	τ ₂	T _o		IN/A
	A	1	2×6	5× 6	3 10.03	3	9		
	В	1	2 × 0 ₅	5 × G _S	13.50	3,38	5.40		
	c	1	2 × G ₈	5 × G _s	26,67	3,33	5,93		
	E	1	$2 \times G_8$ $2 \times G_8$	5 × G _S 5 × G _S	3,80	1,69	2,34		
	F	1	2 × G _S	5 × G ₈	9,52	1,30	2.28		
7	Docume	entatio	n requi	rement	S				P
7.1	Type te	st repo	rt						Р
	The type describe with IEC aspects	e test re ed in this 60255- shall be	port for s standa -1. As a e record	the fund ard shall minimu ed:	ctional be in a im the f	elemer accorda followin	nts ance Ig		P
	• Equipn equipme details s shall be	nent un ent / fun uch as recorde	der test: ction un model r ed as ap	This in ider test number, oplicable	cludes as we firmwa	details Il as sp ire vers	of the ecific sion		Р
	 Test ec calibration 	quipmer on infori	nt: equip mation.	oment n	ame, n	nodel n	umber,		Р
	 Function operation binary in 	onal blo n of the iput and	ck diagr elemer l output	am sho nt includ signals	wing th ing inte with th	e conc eractior e funct	eptual of all ion.		Р
	 Details of measure 	of the i uremen	nput en t being	ergizing used by) quant the fu	ity and nction.	the type		Р
	Details curves/o that have preferab	of the apperation be been by by m	available n for bo impleme eans of	e charac th opera ented in an equa	cteristic ating ar the fur ation.	nd resen nction,	t states		N/A
	• The va curves b	lue of G being im	G _⊤ in the plemen	e case c ted.	of depe	ndent t	ime		N/A
	Details in exces	of the lass of G	behavio	ur of the	e functi	on for c	currents		N/A
	• Details including voltage-	of all sog k 1 , k depend	ettings u 2 , k 3 a ent eler	utilised I and k 4 nents.	by the f in the c	unctior case of	١,		N/A
	Details impleme function performa algorithm for exam sufficien once wit the oper describe	of any ented to to a rea ance cla ns that a nple volt t to des hin the ration of ed.	specific improve al power aims. In are used tage trai cribe the user do all func	algorith e the ap system the cas d by mo nsforme e opera cument ctions th	nms that plicabi n, and t e of ge ore thar er supe tion of ation b at use	at are lity of th heir neric none fu rvision, the algo ut its ef it shall	nis Inction, it is orithm ifect on be		N/A
(LO)	L	k	G)			120)	(xC)	(, (, (, (, (, (, (, (, (, (, (, (, (, (

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Clause	Requirement + Test	Result - Remark	Verdict
	• Test method and settings: This includes details of the test procedure being used as well as the settings that are applied to the equipment under test to facilitate the testing. This may include settings other than those for the function being tested. This permits repeat testing to be performed with confidence that the same test conditions are being used		P
	• Test results: For every test case outlined in the test method and settings, the complete sets of results are recorded as well as a reference to the particular test case. From these results, accuracy claims are established.		P
	• Test conclusions: Based upon the recorded test results, all claims required by Clause 5 of this standard shall be clearly stated. Where appropriate, these claims are compared with the performance specifications contained in this standard to allow individual pass / fail decisions to be given, as well as an overall pass / fail decision for the entire function.		P
7.2	Other user documentation		Р
	Not all users insist on viewing the complete type test documentation, but require a subset of the information that it contains. For this purpose, as a minimum the following aspects shall be recorded in generally available user documentation although this may not be required in a single document:		P
	• Functional block diagram showing the conceptual operation of the element including interaction of all binary input and output signals with the function		Р
	• Details of the input energizing quantity and the type of measurement being used by the function.		Р
	• Details of the available characteristic curves/operation for both operating and reset states that have been implemented in the function, preferably by means of an equation.		N/A
	• The value of G $_{T}$ in the case of dependent time curves being implemented.		N/A
	\bullet Details of the behaviour of the function for currents in excess of G $_{\rm D}$, and its value.		N/A
	• Details of all settings utilised by the function, including k1, k2, k3 and k4 in the case of voltage- dependent elements.		N/A

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Clause	Requirement + Test Result - Remark	Verdict
	Details of any specific algorithms that are implemented to improve the applicability of this function to a real power system, and their performance claims. In the case of generic algorithms that are used by more than one function, for example voltage transformer supervision, it is sufficient to describe the operation of the algorithm once within the user documentation but its effect on the operation of all functions that use it shall be described.	P
	All claims required by Clause 5 of this standard shall be clearly stated.	Р
Annex A	Constants for dependent time operating and reset characteristics	N/A
	Table A.1 shows the constant for dependent time operating and reset characteristics	N/A
	Table A.1 – Constants for dependent time operating and reset characteristicsCurve typeOperating time $t(G) = TMS\left(\frac{k}{\left(\frac{G}{G_S}\right)^{\alpha}-1}+c\right)$ Reset time $t_r(G) = TMS\left(\frac{t_r}{1-\left(\frac{G}{G_S}\right)^{\alpha}}\right)$ Commonly used namekca $t_r(G) = TMS\left(\frac{t_r}{1-\left(\frac{G}{G_S}\right)^{\alpha}}\right)$ ckcat_rsssA0.1400.02B13.501C8002C8002E19.610.491221.6E19.610.491221.62E28.20.1217229.12E28.20.121729.12	N/A
	For curves A, B and C, the manufacturer shall declare if dependent time reset characteristic is implemented and provide the appropriate information.	
Annex B	Reset time determination for relays with trip output only	N/A
B.1	General	N/A
	Measuring relays and protection equipment have different output configurations. For equipment that has only a trip output the determination of a dependent reset time can be achieved by many different methods. The following clause describes an example of such a test method.	N/A
B.2	Test method	N/A

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The determination of the reset time for relays without an appropriate contact can be achieved using the following method to determine a basic accuracy of the reset time. A current of twice the setting is applied to the relay for a pre-determined length of time such that the unit does not operate but will have reached 90 % of its trip value. The current is then reduced instantaneously to a pre-determined value below setting for a fixed time. After this time has elapsed, the current is instantaneously increased to twice the setting value until the element trips. The trip time is determined based on the value of the internal integrator. This is shown graphically in Figure B.1 . The test method is repeated with the applied current being reduced to a different value or each occasion. This generates a range of trip times from which the reset times can be extrapolated and with sufficient points a reset curve can be created.	e e	N/A
Energising quantity Operate signal Value of internal time delay counter Reset Trip time counter IEC 1717/09		N/A
	TESTING CENTRE TECHNOLOGY Page 30 of 30 IEC 60255-151 Requirement + Test The determination of the reset time for relays without an appropriate contact can be achieved using the following method to determine a basic accuracy of the reset time. A current of twice the setting is applied to the relay for a pre-determined length of time such that the unit does not operate but will have reached 90 % of its trip value. The current is then reduced instantaneously to a pre-determined value below setting for a fixed time. After this time has elapsed, the current is instantaneously increased to twice the setting value until the element trips. The trip time is determined based on the value of the internal integrator. This is shown graphically in Figure B.1 . The test method is repeated with the applied current being reduced to a different value or each occasion. This generates a range of trip times from which the reset times can be extrapolated and with sufficient points a reset curve can be created. Image: Operate signal Value of internal time for setting Value of internal time diag counter Image: time setting Value of internal time Image: time Value of internal time Image: tima	TEETING CENTRE TECHNOLLOY Page 30 of 30 Report No.:T IEC 60255-151 IEC 60255-151 Requirement + Test Result - Remark The determination of the reset time for relays without an appropriate contact can be achieved using the following method to determine a basic accuracy of the reset time. A current of twice the setting is applied to the relay for a pre-determined length of time such that the unit does not operate but will have reached 90 % of its trip value. The current is then reduced instantaneously to a pre-determined value below setting for a fixed time. After this time has elapsed, the current is instantaneously increased to twice the setting value until the element trips. The trip time is determined based on the value of the internal integrator. This is shown graphically in Figure B.1. The test method is repeated with the applied current being reduced to a different value on each occasion. This generates a range of trip times from which the reset times can be extrapolated and with sufficient points a reset curve can be created. Usue of internal time setting output the element trips. The test method is repeated with the applied current being reduced to a different value on each occasion. This generates a range of trip times from which the reset times can be extrapolated and with sufficient points a reset curve can be created. Usue of internal time Immensity trip Usue o





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Photo 5-External view





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Photo 7-Internal view









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Photo 11-Internal view

